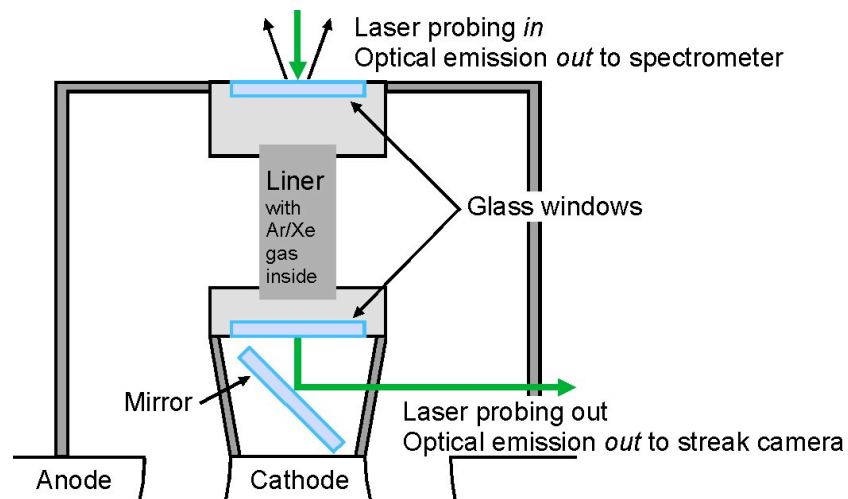


Gas-filled Cylindrical Liner Experiments on MAGPIE

Outline of experiment



System is **diagnosed 'end-on'** along the liner axis

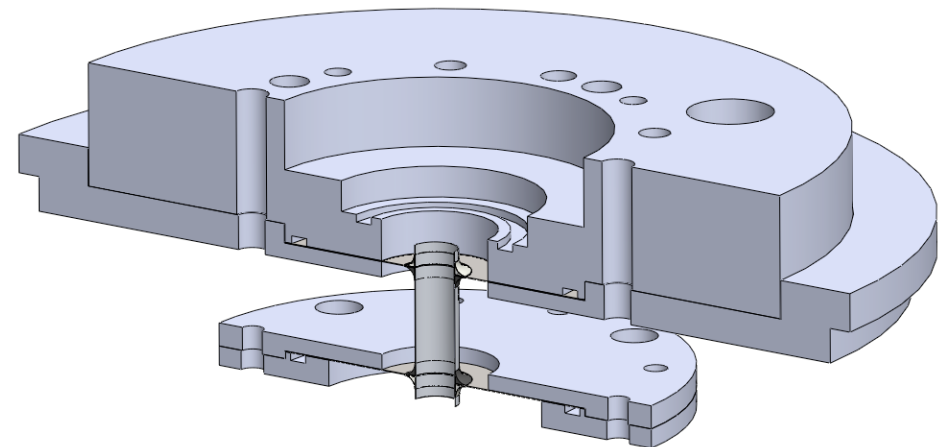
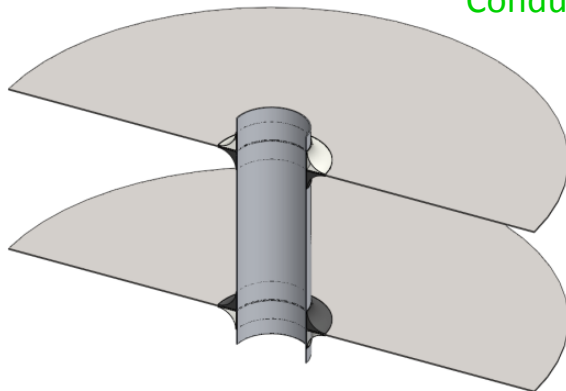
- 355nm (UV) and 532nm interferometry and Schlieren imaging
- Optical streak photography
- Optical spectroscopy

Electrical contacts to load hardware

14mm

Liner

Conducting silver paint
Epoxy



Outline of experiment

1.4 MA, 250 ns current pulse is delivered to a **gas-filled cylindrical liner**

Aluminium Liners

6 mm diameter, 80 μm wall

Aspect Ratio = 40

14 mm long

Al 6061

$$\delta_0 = \sqrt{2\rho/\mu} = 60\mu\text{m}$$

- Multiple shocks driven into gas from inner liner surface
- Shocks are radiative – evidence for precursor
- No bulk motion of the liner wall
- No plasma seen on outer liner surface

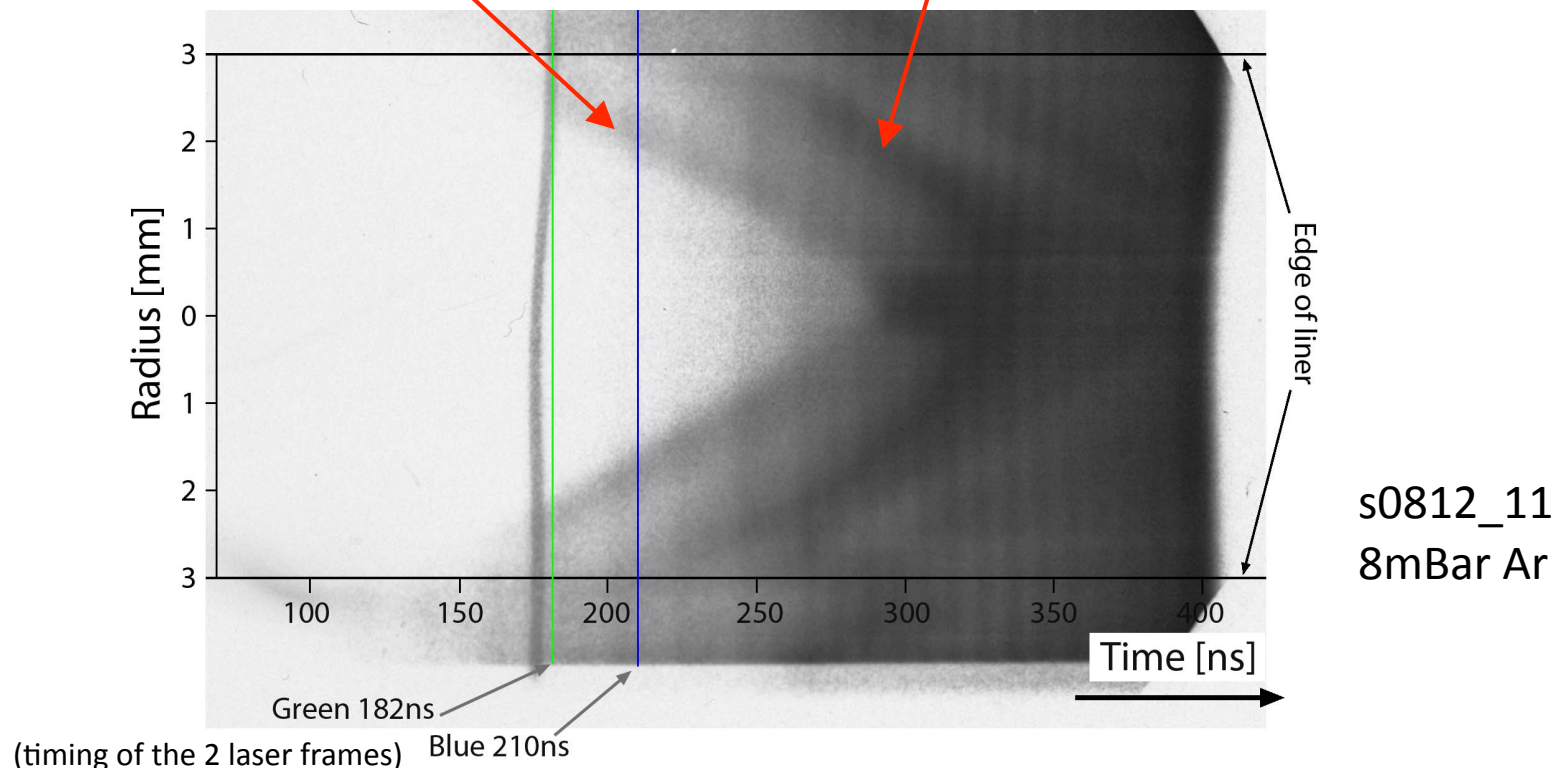
Gas	$\rho = 1.2\text{e-}6 \text{ g/cc}$	$\rho = 6\text{e-}6 \text{ g/cc}$	$\rho = 1.3\text{e-}5 \text{ g/cc}$
Argon (A=40, Z=18)	0.7mBar ($1.8\text{e}16\text{atoms/cc}$)	--	8mBar ($2\text{e}17\text{atoms/cc}$)
Xenon (A=131, Z=54)	--	1.1mBar ($2.7\text{e}16\text{atoms/cc}$)	2.5mBar ($6\text{e}16\text{atoms/cc}$)
Nitrogen (A=14, Z=7)	--	--	15mBar (N_2) ($7.3\text{e}17 \text{ atoms/cc}$)

Results (i) Shock dynamics in gas-filled cylindrical aluminium liners

Dynamics from optical streak camera

1st shock - almost linear trajectory. $V = 20 \text{ km/s}$.
Blow-off from inner surface of liner is pushing into cold, neutral argon gas, ionising and heating it.

2nd shock is launched into heated, ionised argon. **Accelerating trajectory** may indicate presence of current and B field inside the liner.

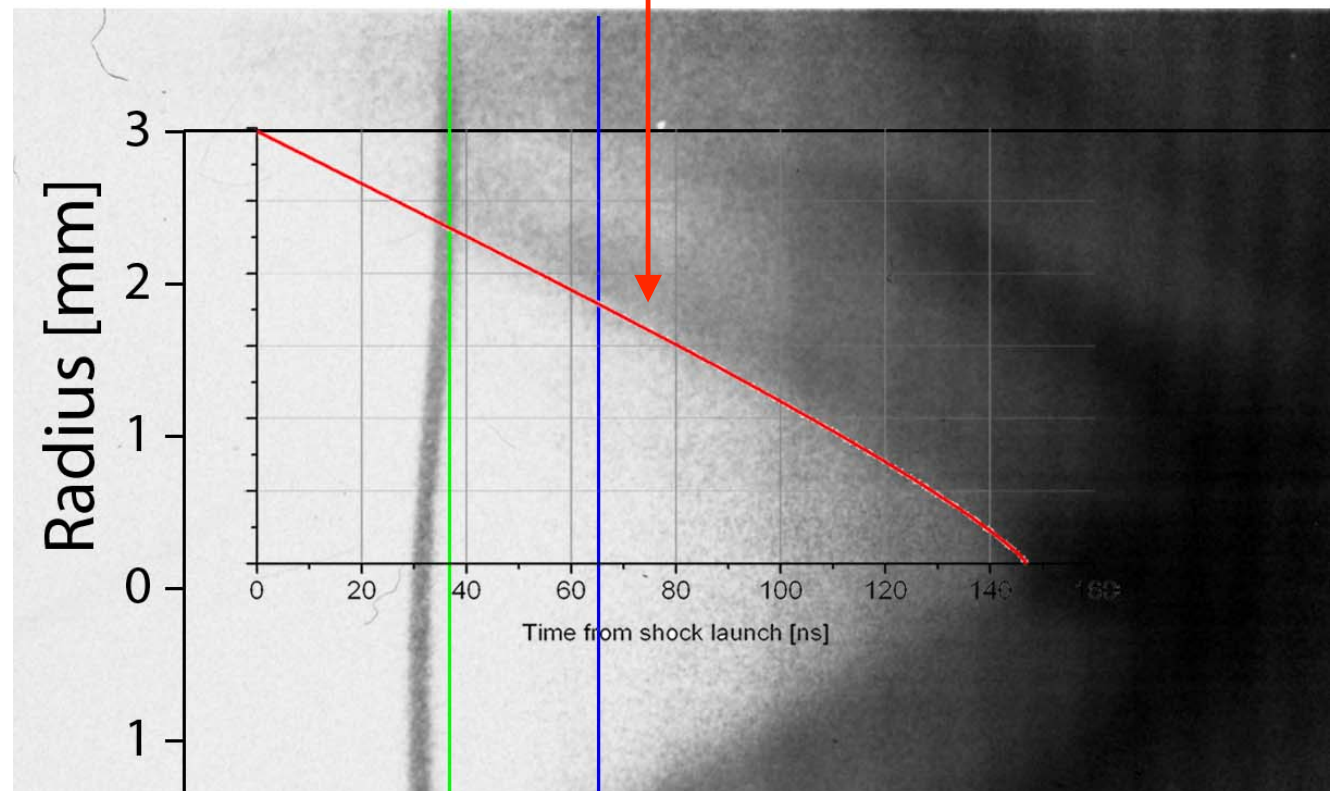


Shock trajectories

1st shock trajectory consistent with analytic solution (**red line**) for converging shocks caused by a cylindrical piston motion (Guderley, 1942):

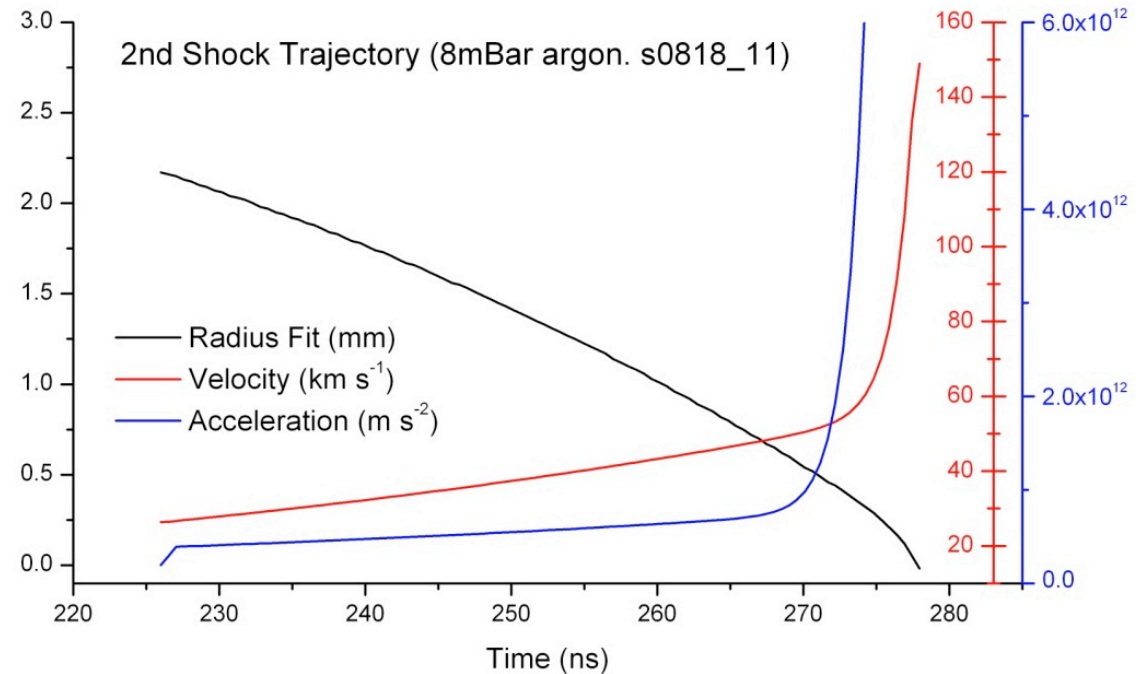
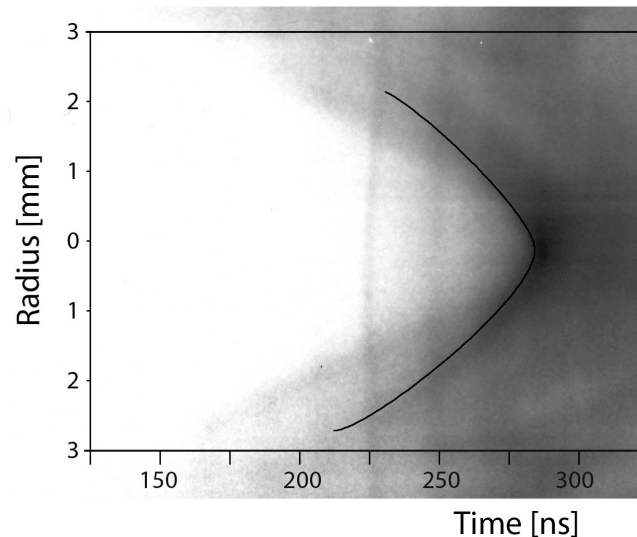
$$R(t) \approx \sum_{i=1} A_i \left(1 - \frac{t}{t_c}\right)^{\alpha_i}$$

Slight acceleration due to converging geometry.



Shock trajectories

Second shock shows more acceleration; driving force could be magnetic field.



Estimate of current in gas

Mass is assumed to occupy a thin shell and is estimated from interferometry line-outs

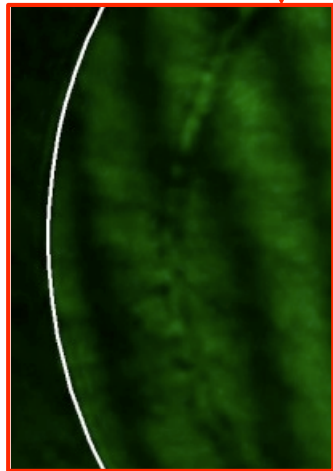
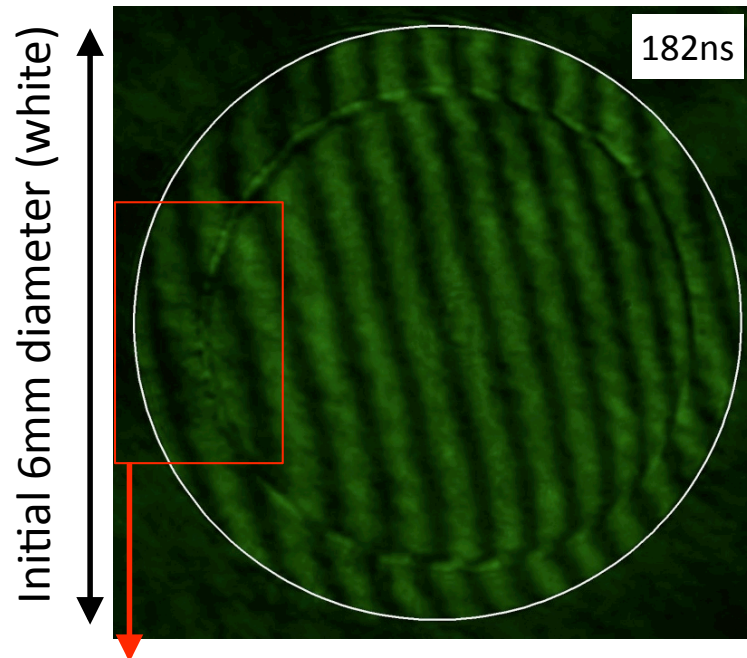
Then, use $F = \text{Magnetic Pressure} \times \text{Area enclosing shell} = ma$

Assuming electron density is due to singly ionised argon atoms, current required for observed acceleration at 253ns is approx. 50 kA

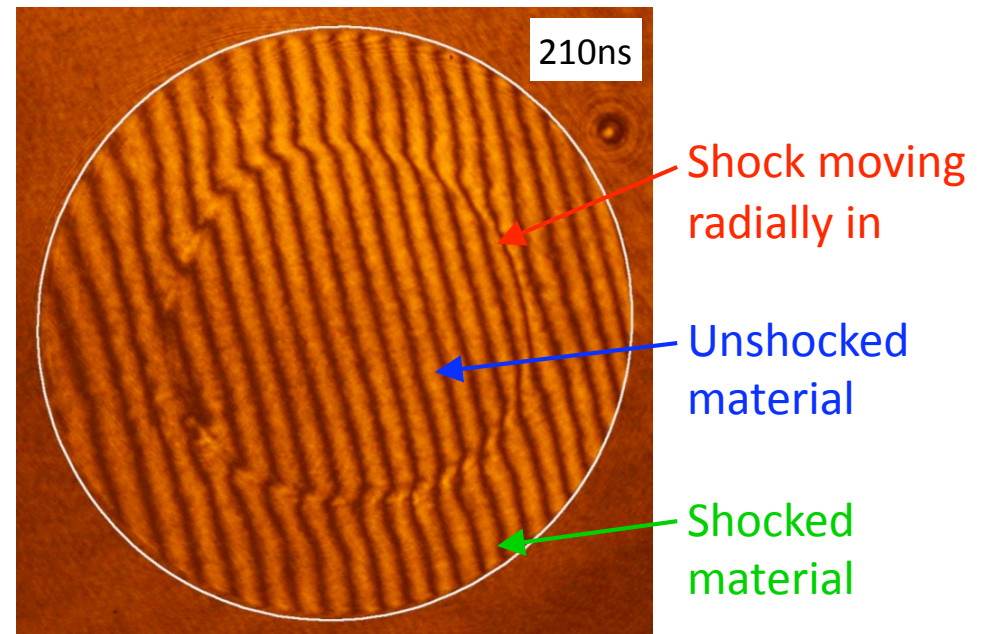
1st shock interferometry (Ar)

There are **two interferometry frames per shot**. One 532nm (green images) and one 355nm (orange images). The inter-frame time is 28ns on all shots.

Data from 8mBar argon shot. s0812_11



Shadowgraphy effect shows up shock structure



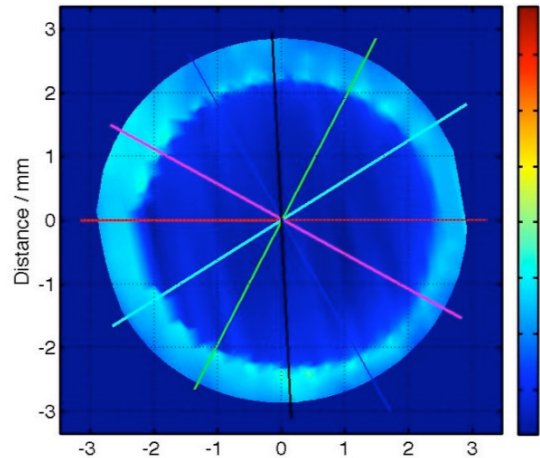
Changes in **electron** and neutral atom line density shift the interference fringes (in opposite directions)

532nm probe is 10X more sensitive to n_e

355nm probe is 5X more sensitive to n_e

1st shock interferometry (Ar)

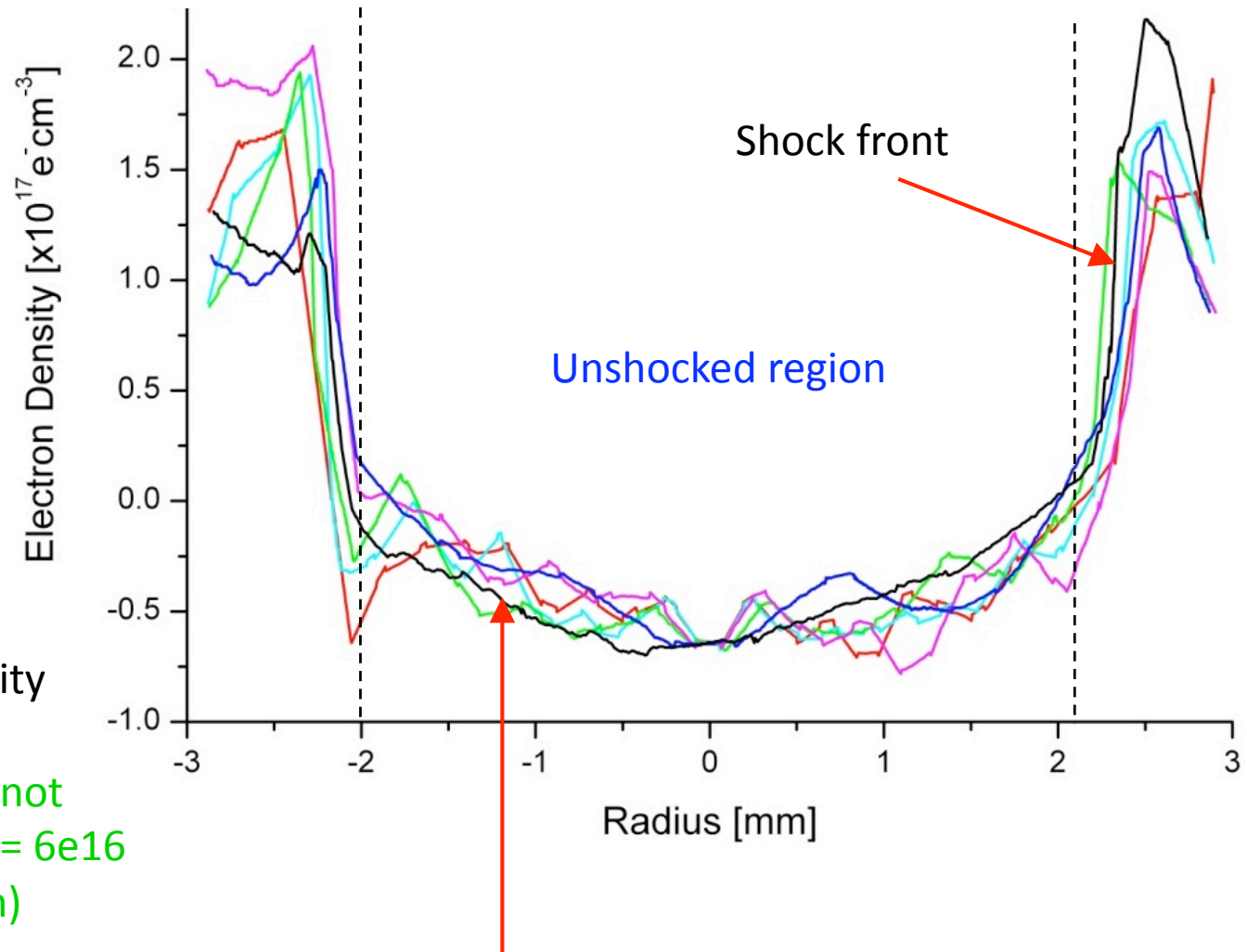
Electron density map from 532nm
frame and position of line-outs



Initial $n_{\text{atom}} = 2 \times 10^{17} \text{ cm}^{-3}$
- matches peak electron density

Position of zero fringe shift is not
known (1 fringe shift gives $n_e = 6 \times 10^{16}$
 cm^{-3} for 532nm, 14mm length)

Line-outs from 532nm electron density map

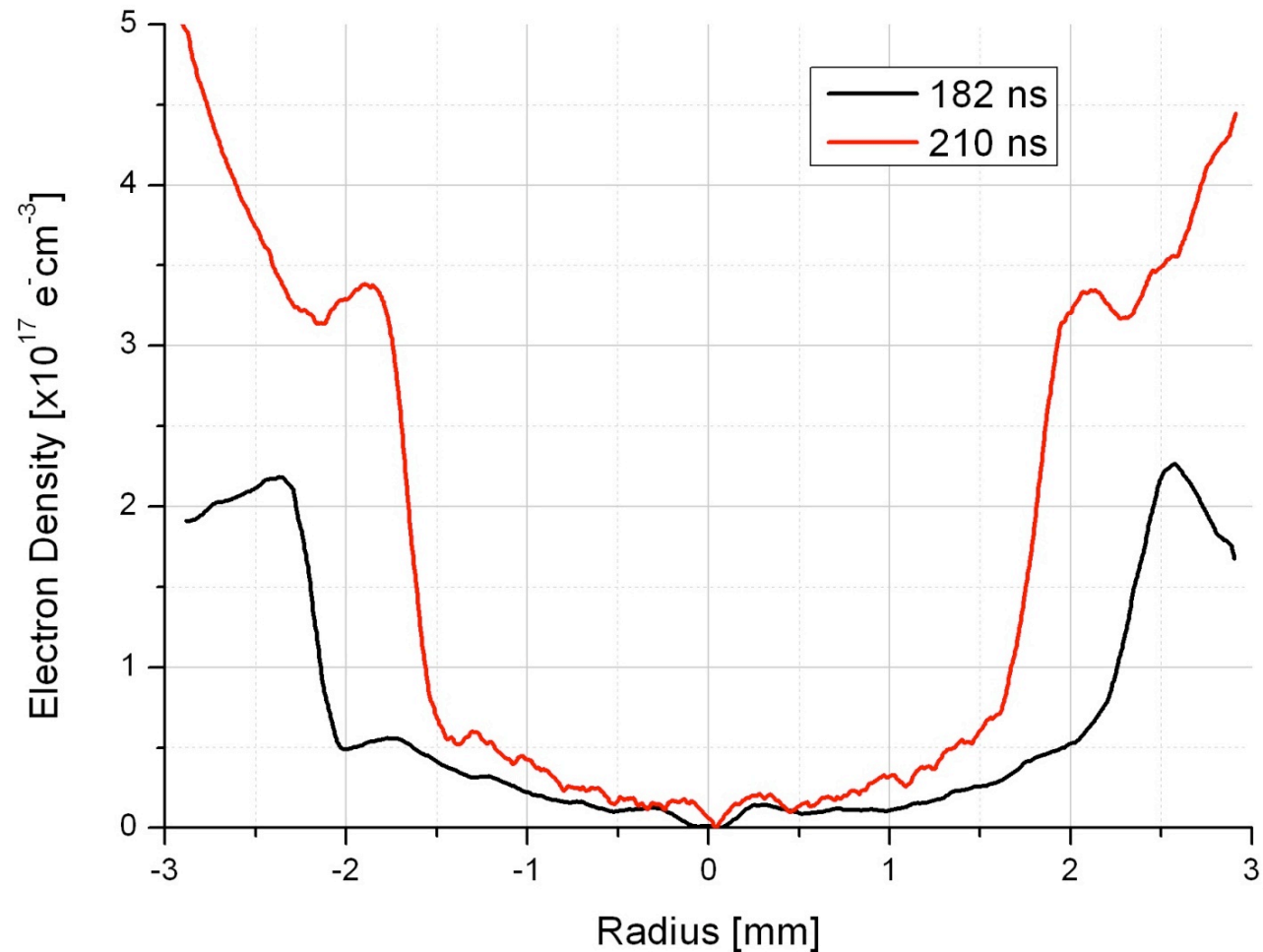


Curved electron density profile in unshocked region – radiative precursor
Consistent with condition for radiative effects

$$\sigma T_s^4 > \rho_0 u_s^3 / 2$$

1st shock interferometry (Ar)

Azimuthally-averaged radial electron density profiles

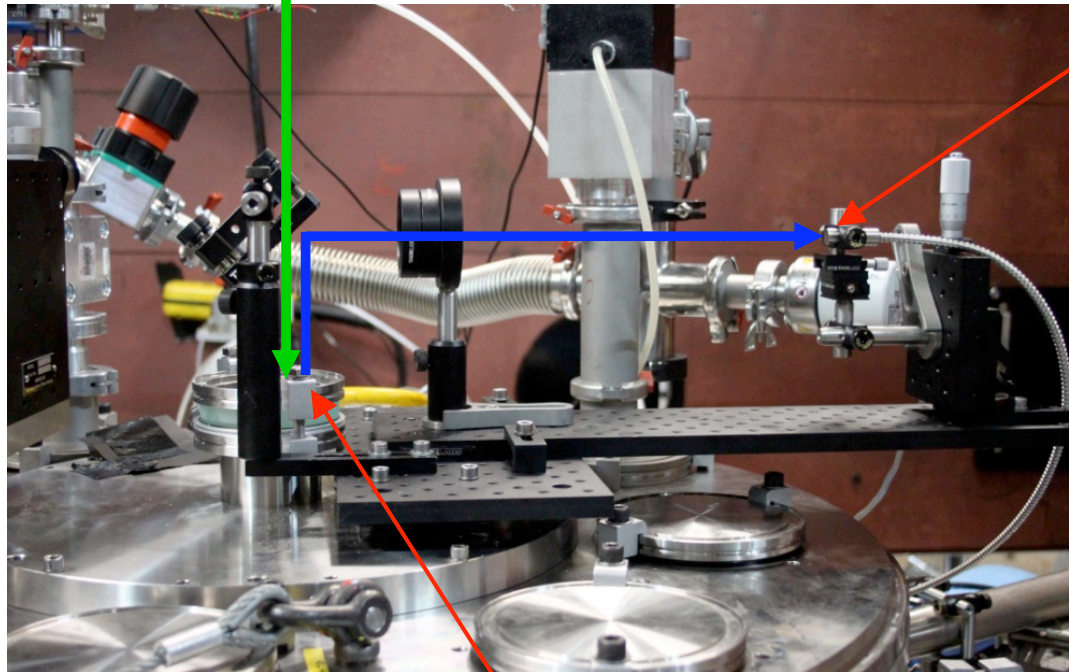


- Axial density has been set to zero. Absolute n_e changes for each lineout remain correct
- Precursor is seen
- Peak electron density increases as shock propagates

Optical spectroscopy

End-on view of liner is imaged onto a 7-fibre bundle and fed to an Andor ½ m spectrometer

Laser probing in



Fibre bundle

Optical emission *out*

Axial window on chamber lid

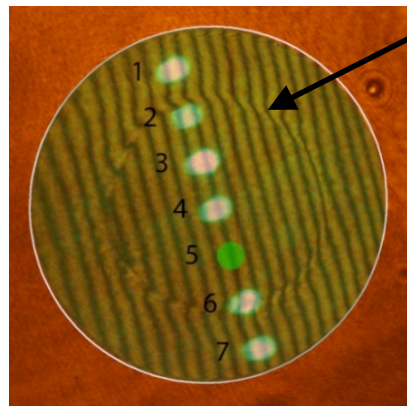
300 lines/mm grating used to give broad range of wavelengths

Corresponding 1nm spectral resolution

Spatial resolution of 800µm from opening angle of collecting lens

Optical spectroscopy

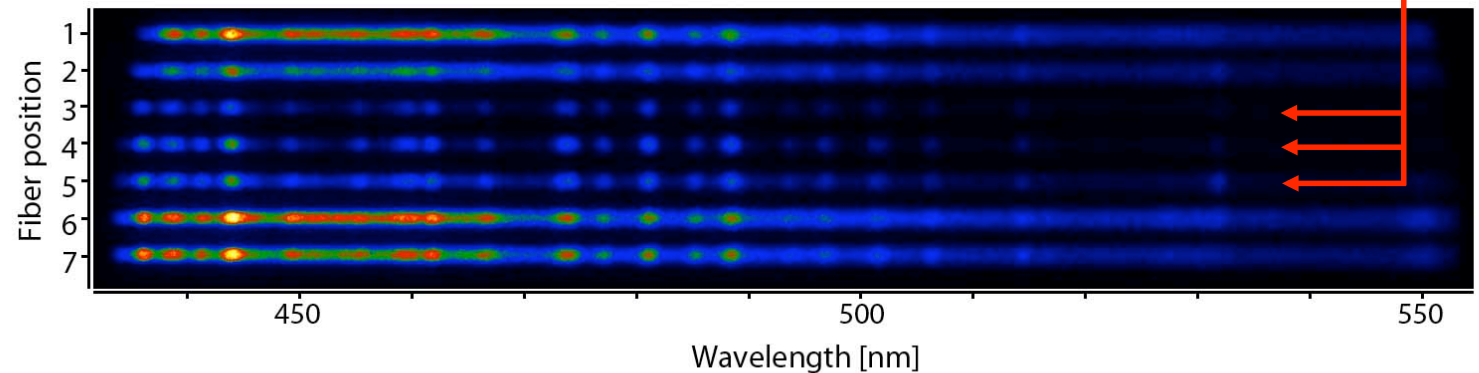
Argon fill (8mBar. S0812_11)



Position of fibres

1st shock, yet to reach axis

Fibres 3, 4 and 5 should collect light from inside the radius of the shock



Majority of lines appear to be ArII

Could be seeing preheating of the unshocked region by radiation from the shock front

Little evidence for Al emission – it is cold and/or there is not much of it

Theoretical post-shock temperature of 2eV given by
agrees with spectroscopic data

$$k_B T_s = \frac{2(\gamma-1)}{(\gamma+1)^2} u_s^2 \cdot \frac{A m_p}{(Z+1)} \quad (\text{P. Drake})$$

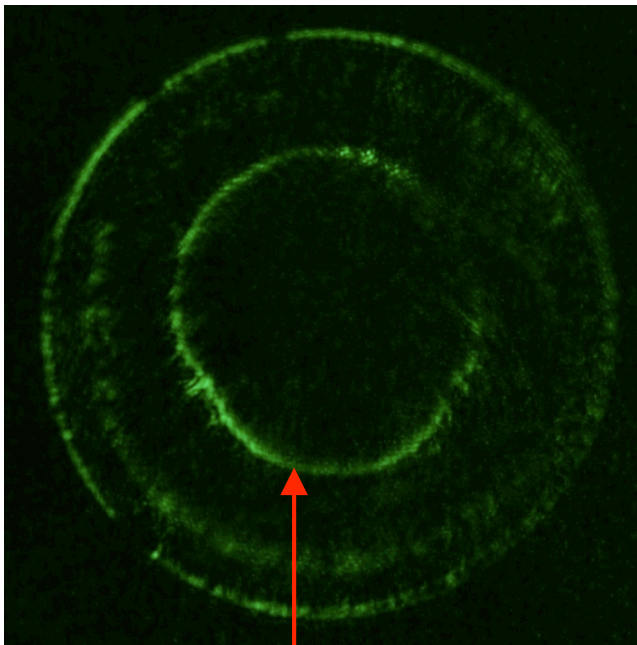
Same general picture when looking at 1st shock in xenon

Later time spectroscopy (of second shock) shows a lot of continuum emission

Schlieren imaging

Schlieren technique is good for imaging the sharp density gradients that occur at shock fronts

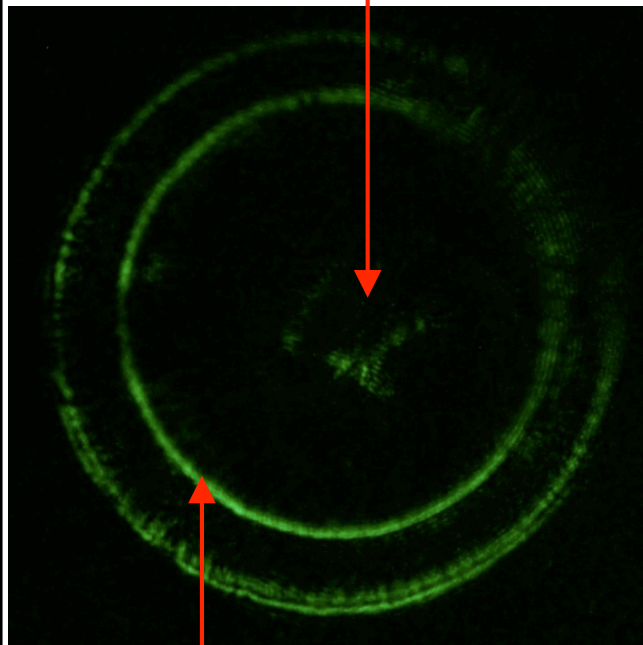
8mBar argon s0818_11



1st shock imaged clearly in
8mBar Ar

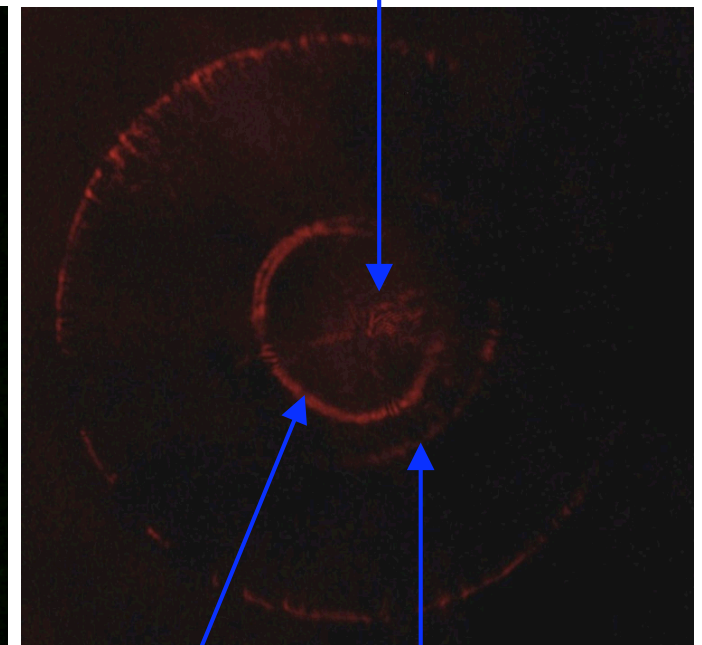
1st shock about to reach the
axis not imaged well for the
lower initial gas density in
this shot

1.1mBar xenon s0823_11



2nd shock is very uniform

Material already on
axis is not well imaged



2nd shock
3rd shock? (not seen on streak)

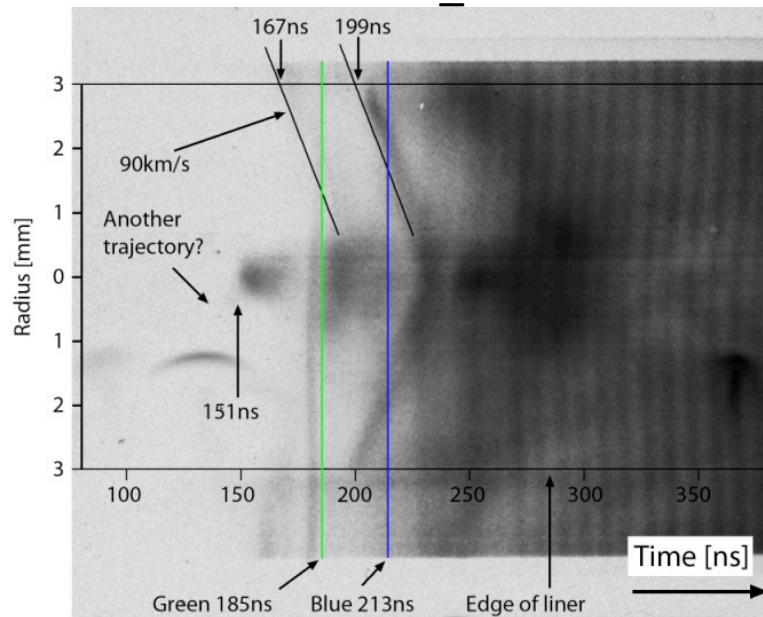
Changing the mass density of the gas

Decreased the mass density of the gas inside to increases the speed of the shocks - more likely to see radiative effects.

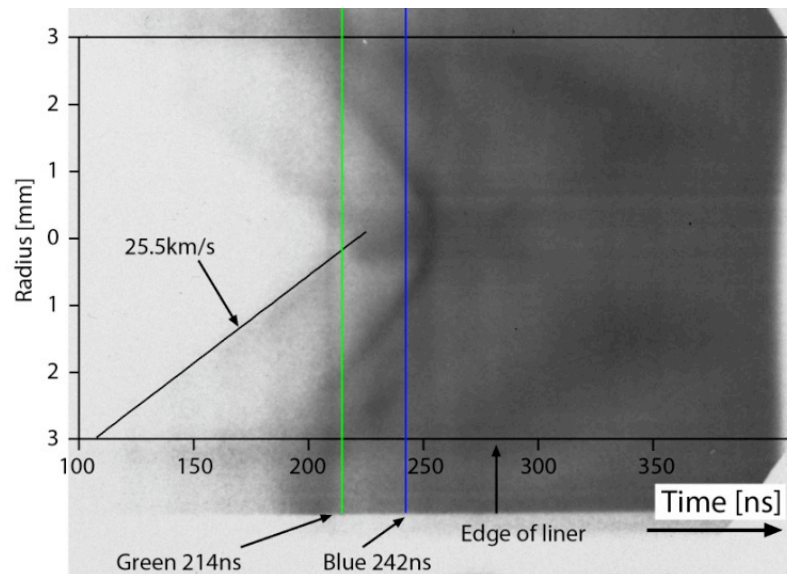
BUT – Shock speed not a strong function of gas density.

System gets difficult to diagnose at low densities as there is less emission and the sensitivity of the interferometer and Schlieren systems is reduced.

0.7mBar Ar. s0810_11



1.1mBar Xe. s0823_11



Shock speed hardly changes when mass density is halved.

Introduce axial magnetic field?

Ram pressure of shock given by $P_{ram} = \rho v^2$

For 1st Ar shock $P_{ram} = 100$ Bar

For 2nd Ar shock $P_{ram} = 1.6$ kBar

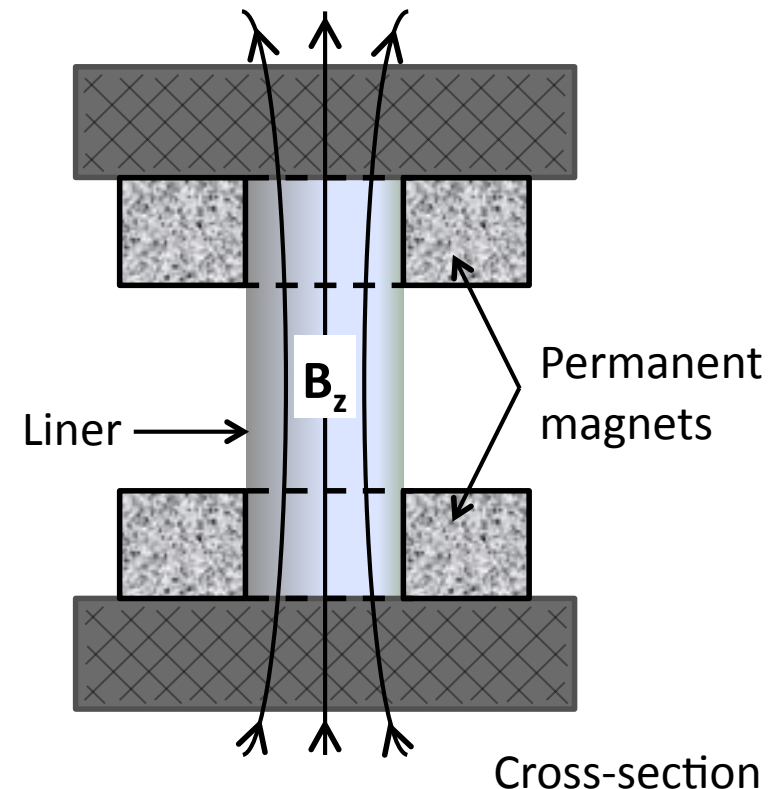
Magnetic pressure given by $P_{mag} = \frac{B^2}{2\mu_0}$

For $P_{mag} = P_{ram}$

$B = 5$ T (1st shock)

$B = 20$ T (2nd shock)

$B \approx 1$ T possible with permanent magnets

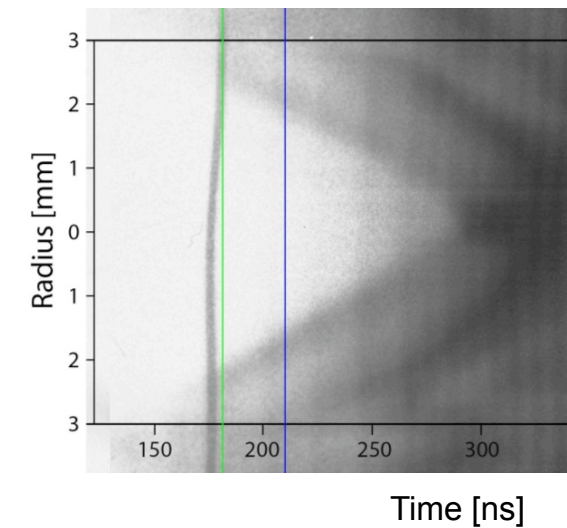
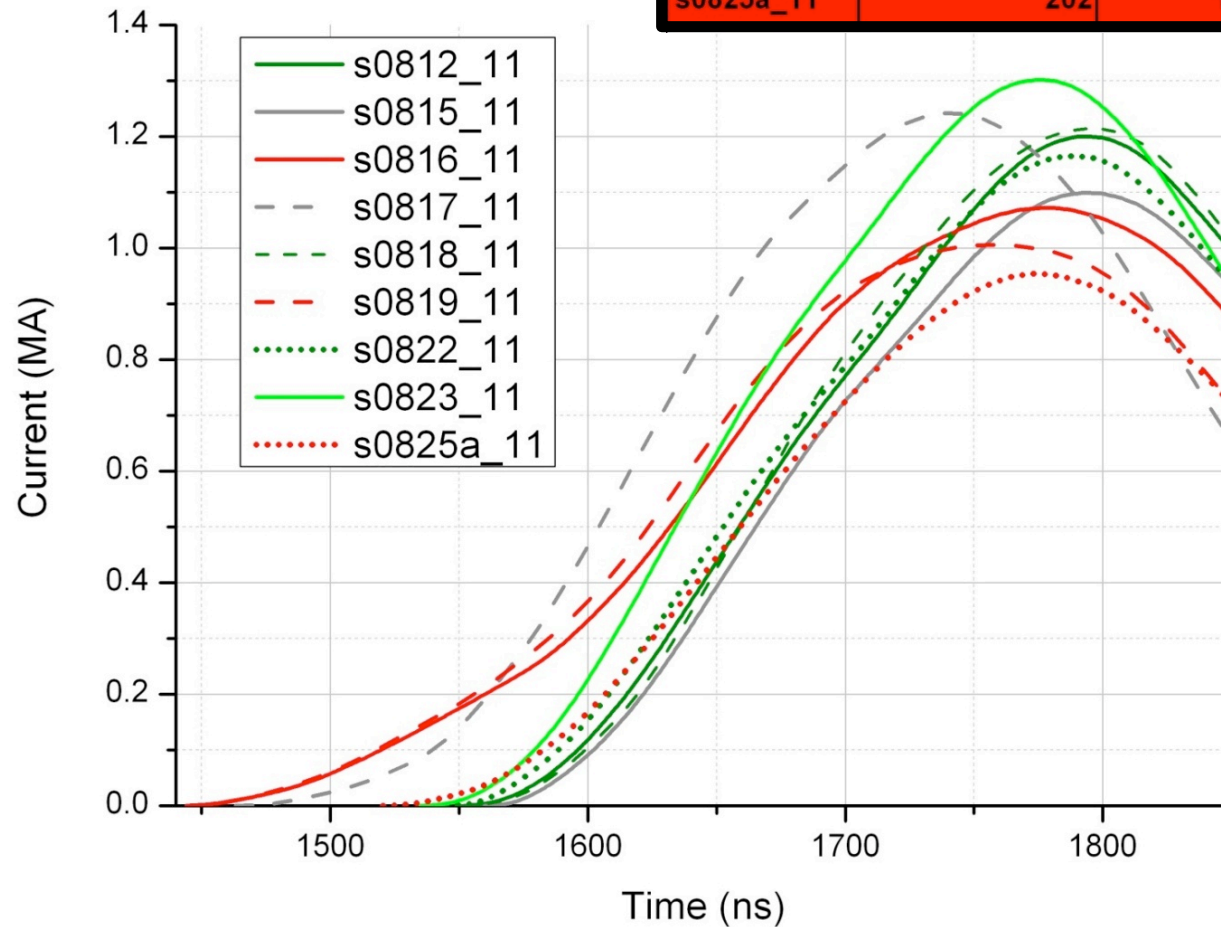


Results (ii)

Shock timing and
current profile

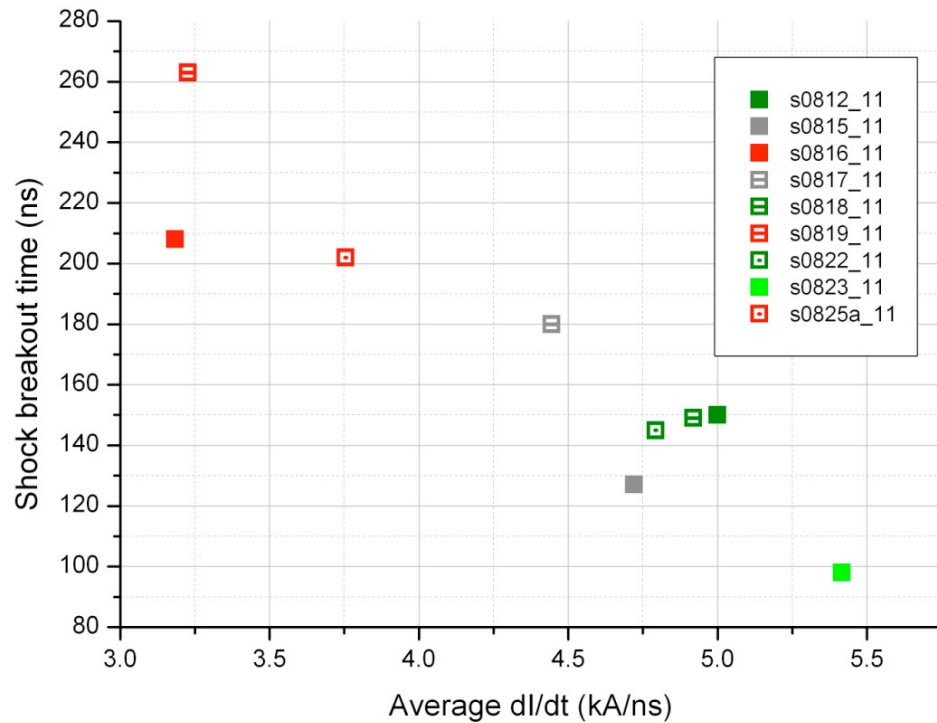
Timing of 1st shock

Shot	1st shock timing ns	Current start ns	Rise ns	Peak current MA	Average di/dt kA/ns	I(t_shock) MA
s0812_11	150	1552	240	1.20	5.00	0.78
s0815_11	127	1560	233	1.10	4.72	0.65
s0816_11	208	1444	336	1.07	3.18	0.63
s0817_11	180	1463	279	1.24	4.44	0.82
s0818_11	149	1550	246	1.21	4.92	0.80
s0819_11	263	1445	313	1.01	3.23	0.94
s0822_11	145	1545	242	1.16	4.79	0.74
s0823_11	98	1535	240	1.30	5.42	0.49
s0825a_11	202	1520	253	0.95	3.75	0.83

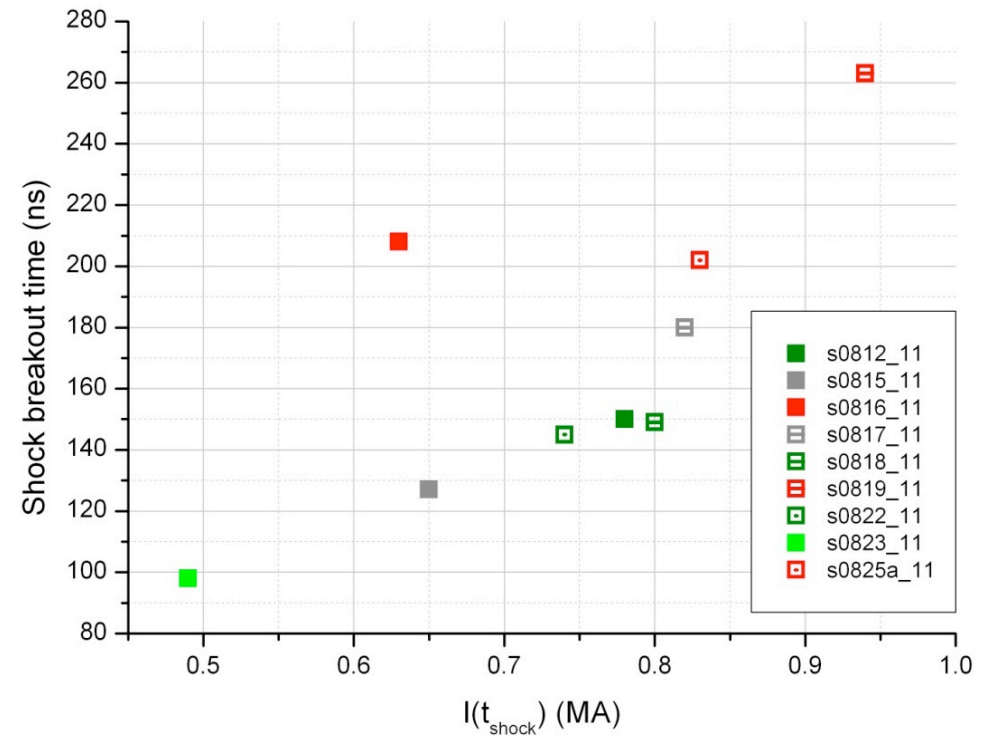


Timing of 1st shock

Shock Timing vs. Average di/dt



Shock Timing vs. Current at Breakout



Timing of 1st shock

Current integral:

$$J = \int_0^t j^2 dt = \int_{Q_0}^{Q_f} \sigma dt$$

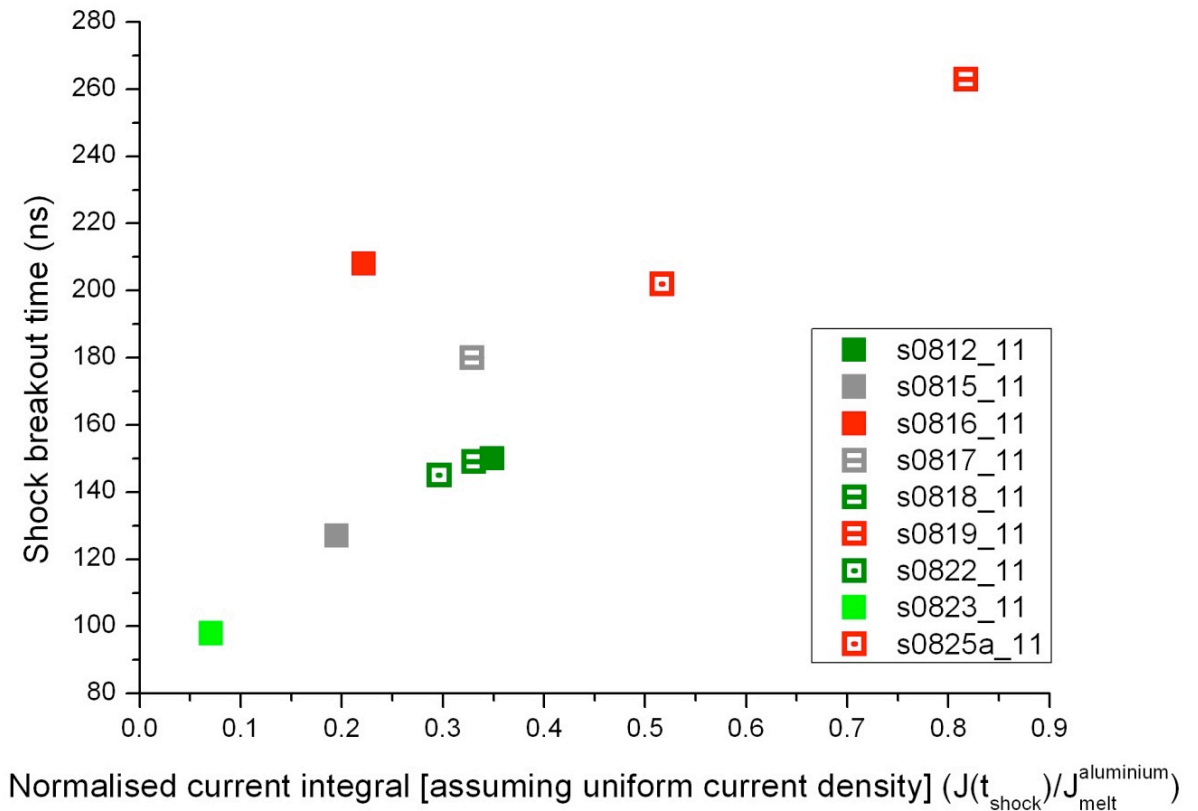
For Al: $J_{solid}^{melt} = 0.32 \times 10^{17} \text{ A}^2 \text{ s m}^{-4}$

$$J_{liquid}^{melt} = 0.40 \times 10^{17} \text{ A}^2 \text{ s m}^{-4}$$

$$J_{liquid}^{boil} = 0.59 \times 10^{17} \text{ A}^2 \text{ s m}^{-4}$$

$$J_{vapor}^{boil} = 1.09 \times 10^{17} \text{ A}^2 \text{ s m}^{-4}$$

(Knoepfel, Wiley)



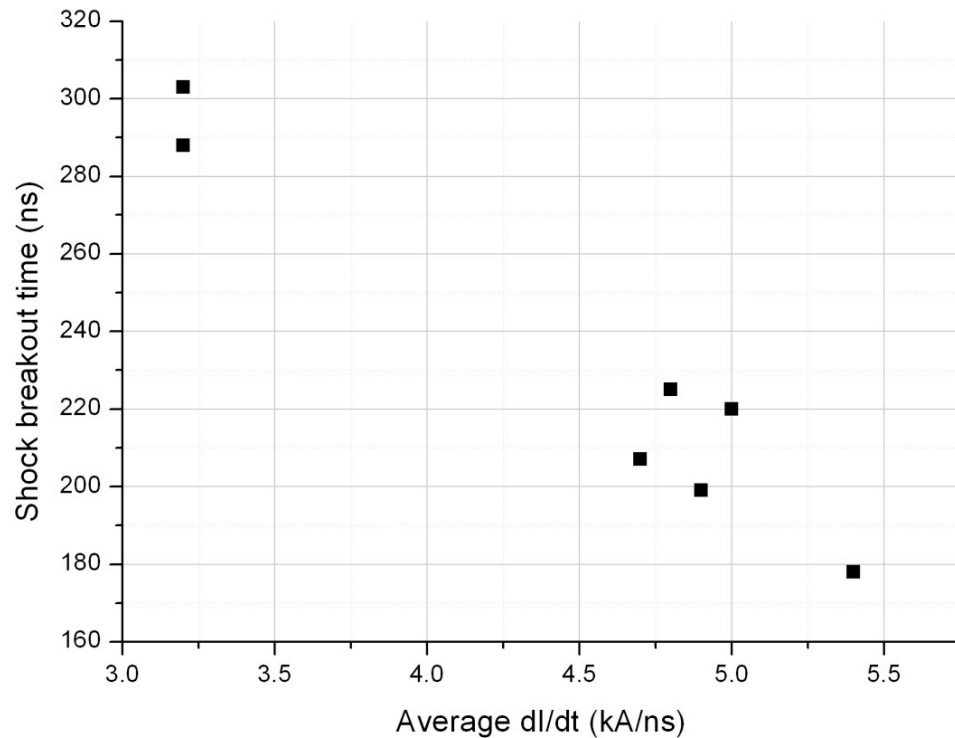
Calculated current integral at t_{shock} from measured current signal

Assumed uniform current density

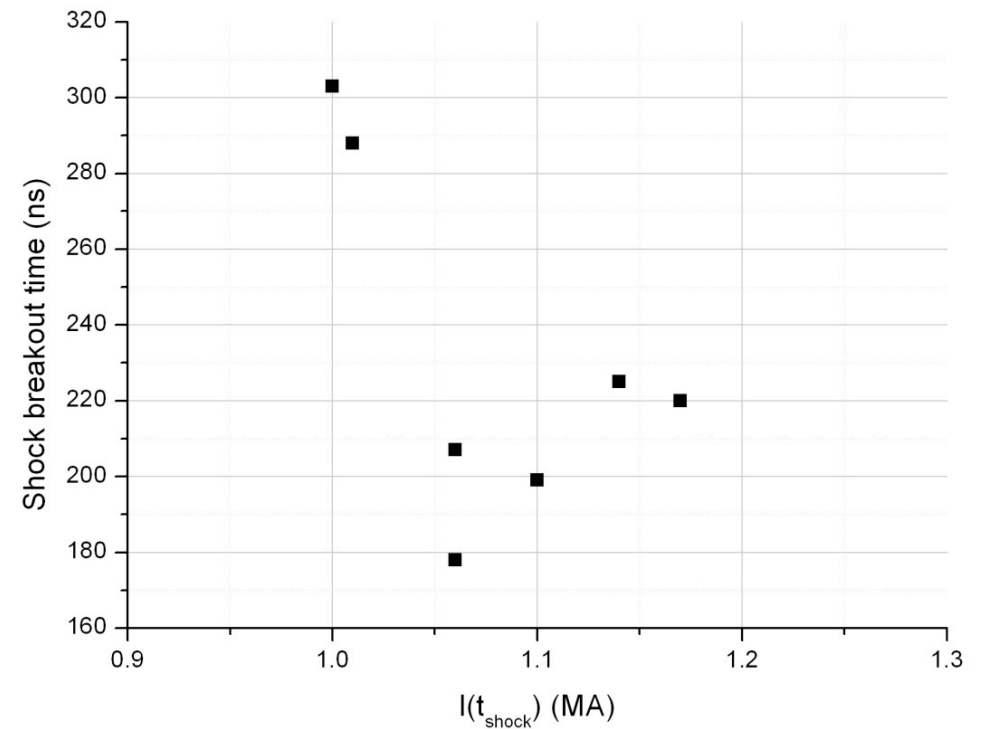
Normalised to J_{solid}^{melt}

Timing of 2nd shock

Shock Timing vs. Average di/dt

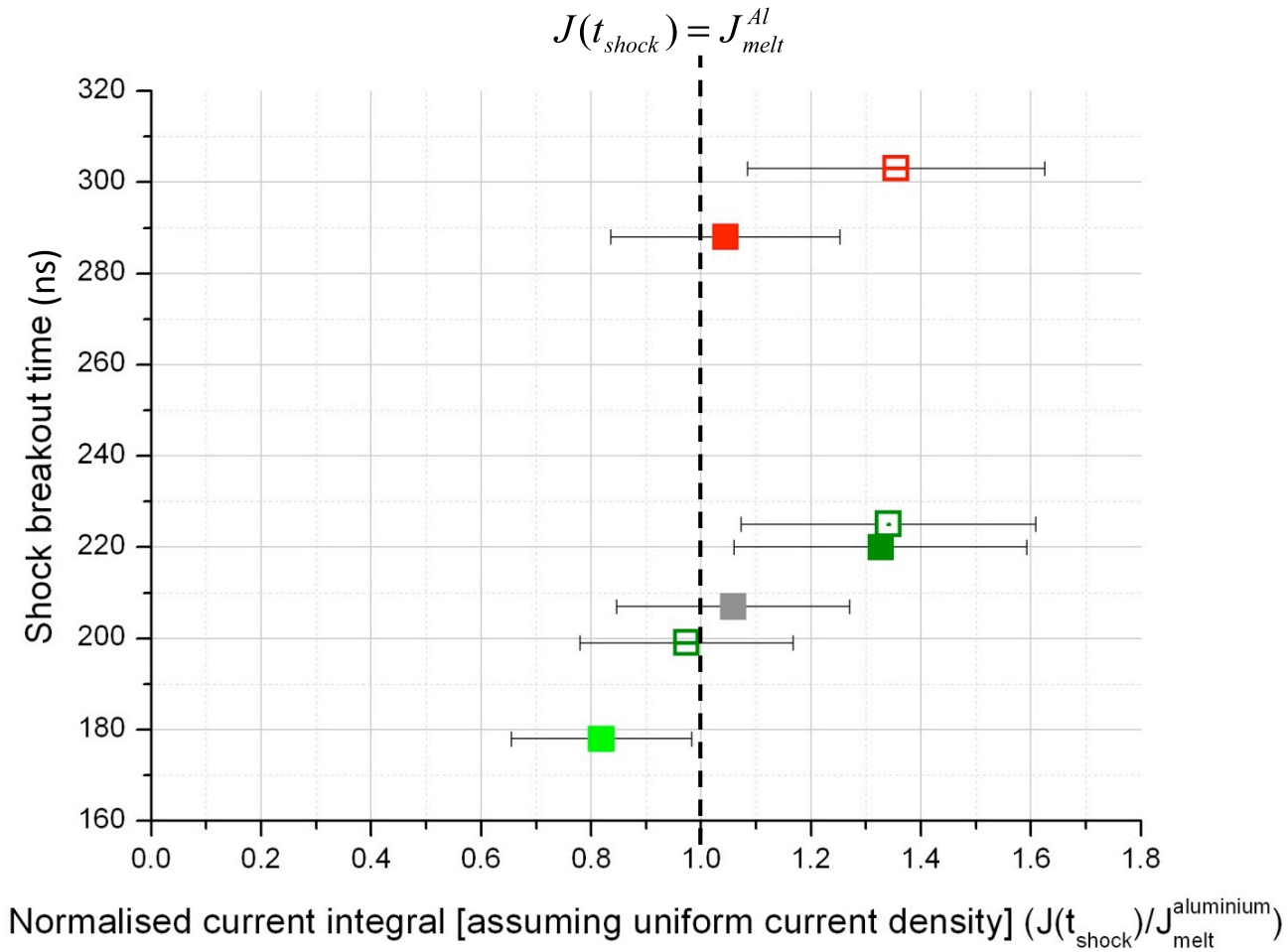


Shock Timing vs. Current at Breakout



Timing of 2nd shock

Current integral for 2nd shock



Results (iii)

Observations of
outer liner surface

Outline of experiment

1.4 MA, 250 ns current pulse is delivered to a **cylindrical liner**

Aluminium Liners

6 mm diameter, 80 μm wall

Al 6061

$$\delta_0 = \sqrt{2\rho/\mu} = 60\mu\text{m}$$

Homemade Aluminium Liners

10/14 mm diameter, 20 μm wall

Al kitchen foil

$$\delta_0 = \sqrt{2\rho/\mu} = 60\mu\text{m}$$

Nickel Liners

3.6 mm diameter, 50 μm wall

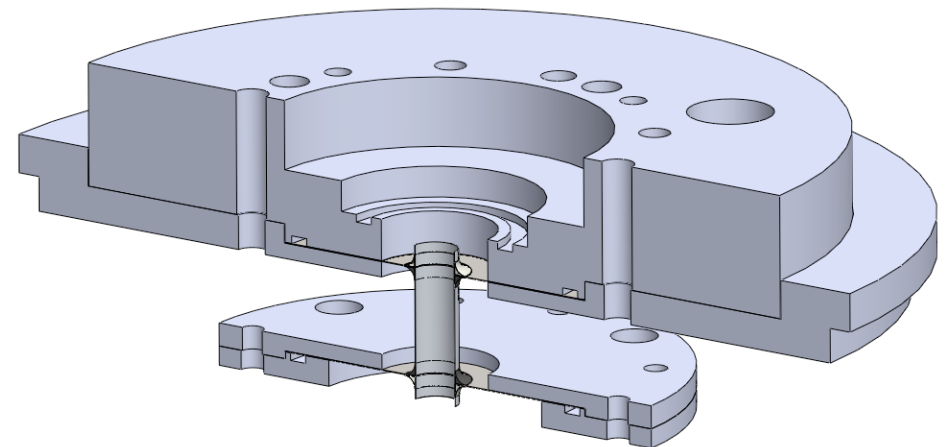
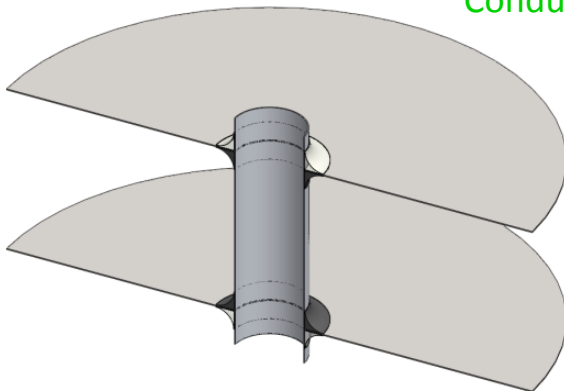
$$\delta_0 = \sqrt{2\rho/\mu} = 90\mu\text{m}$$

Electrical contacts to
load hardware

14mm

Liner

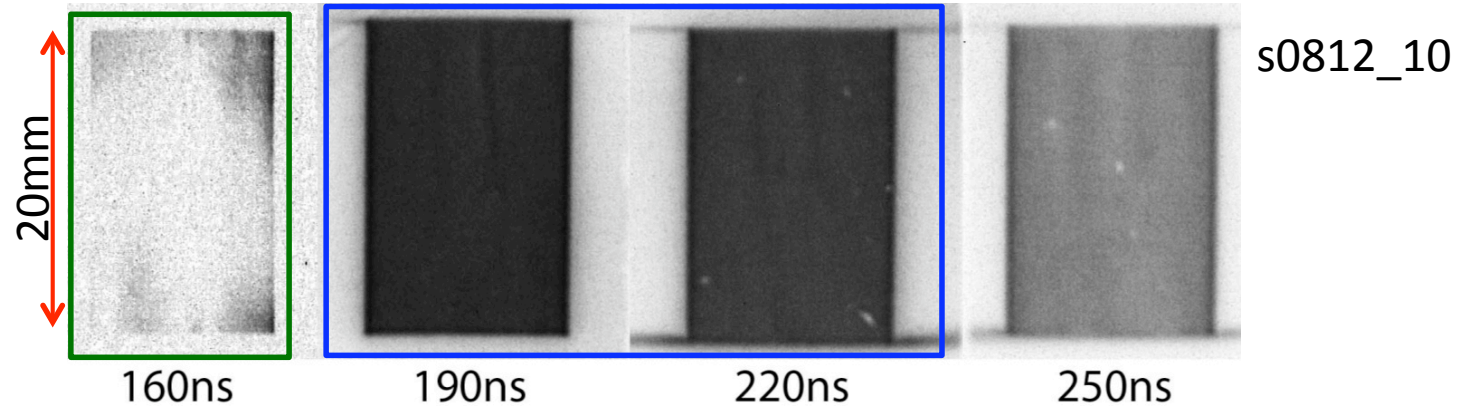
Conducting silver paint
Epoxy



Imaging the outside surface of liners

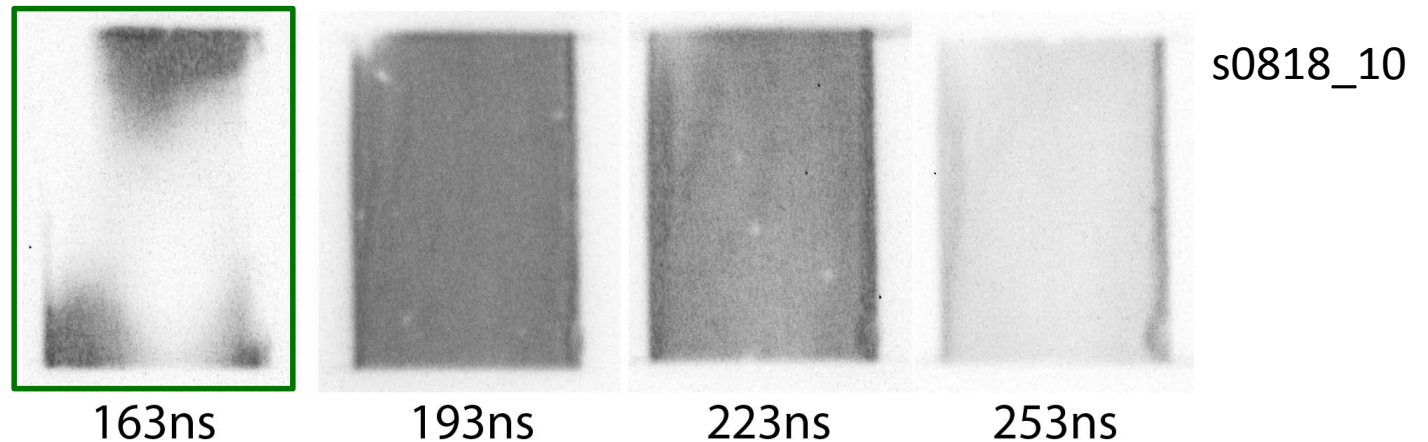
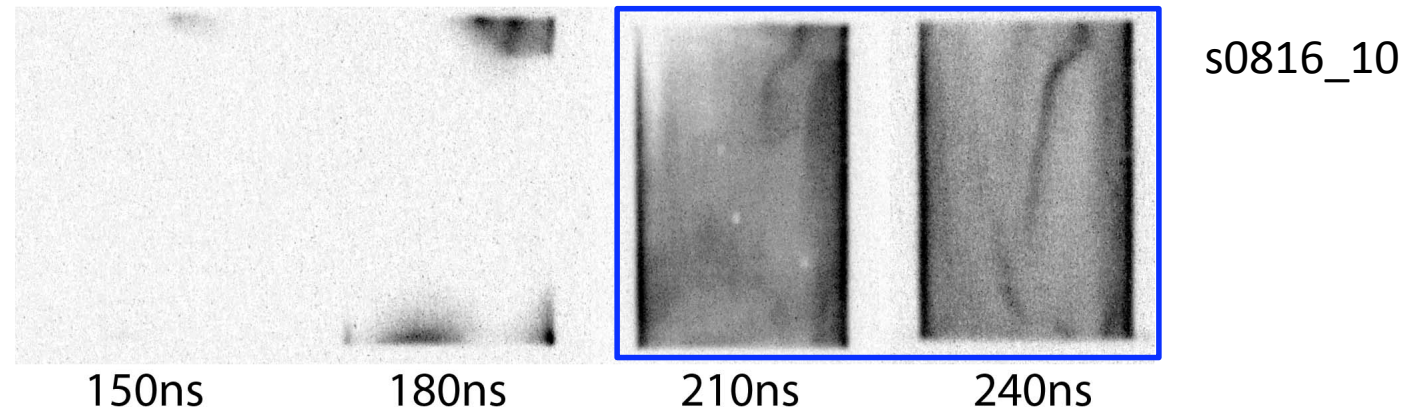
XUV pinhole images

20 μ m wall
homemade Al liners



Start-up at both ends

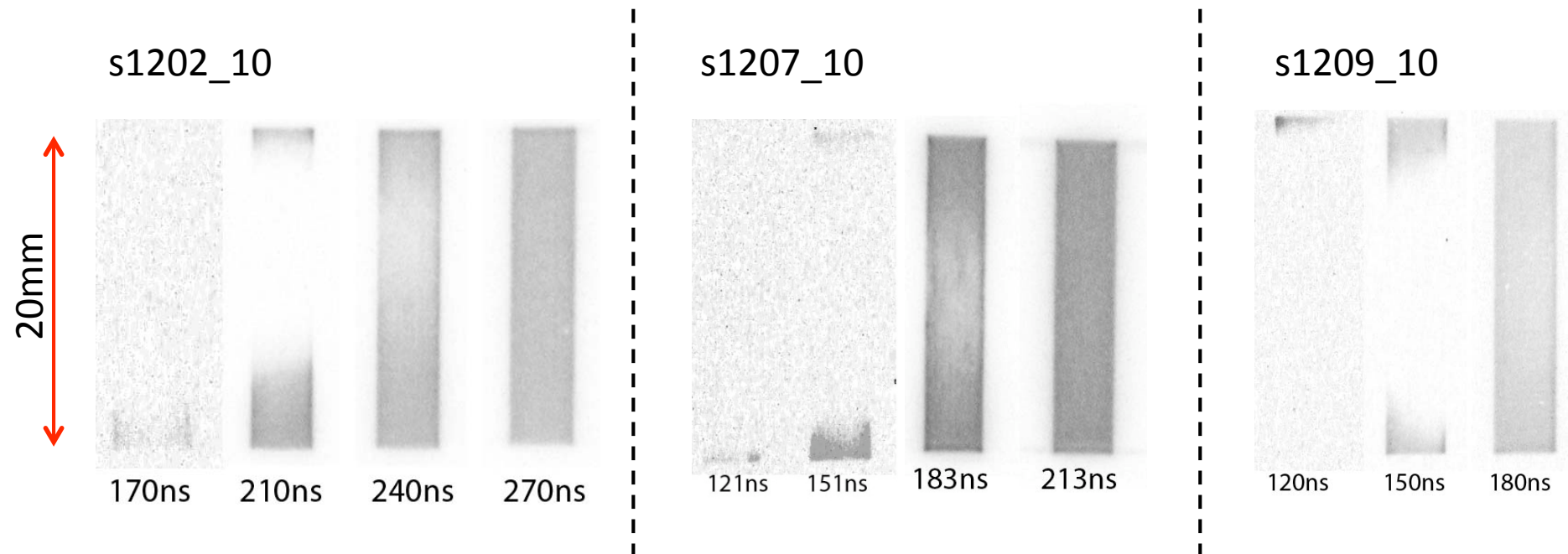
Striation often seen on
homemade liners



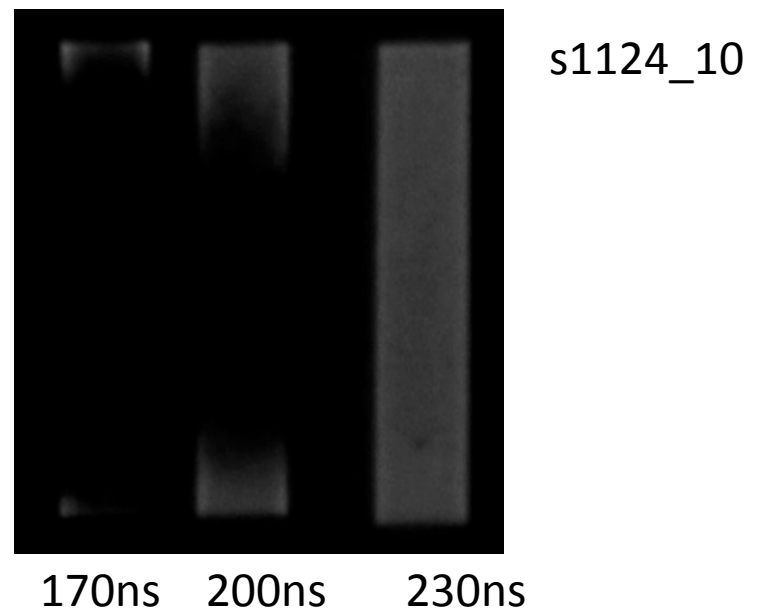
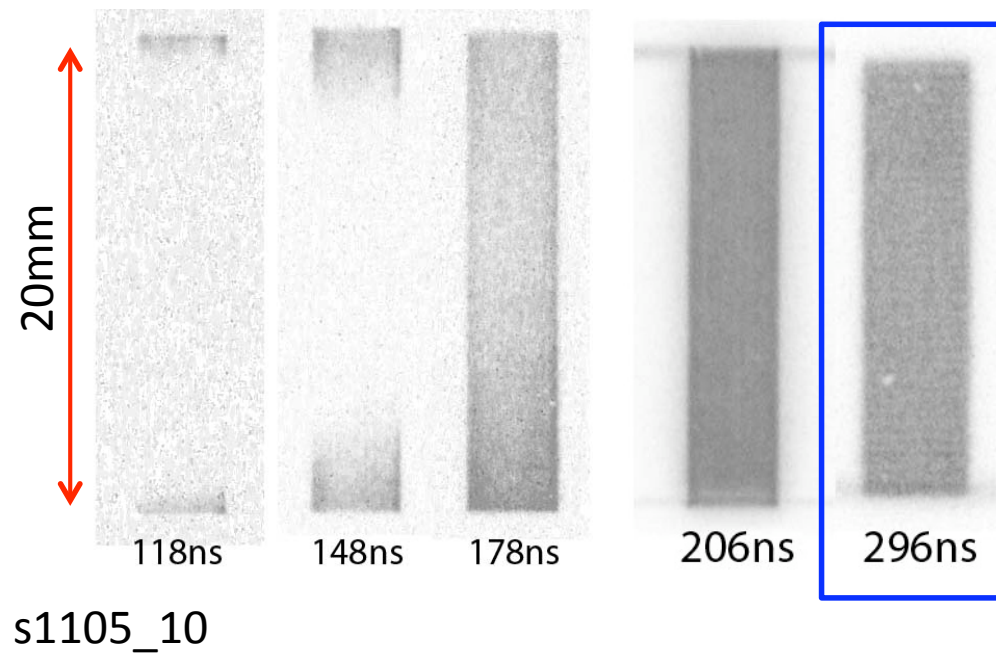
Imaging the outside surface of liners

XUV pinhole images

50 μ m wall, 3.6mm OD Ni liners



Imaging the outside surface of liners

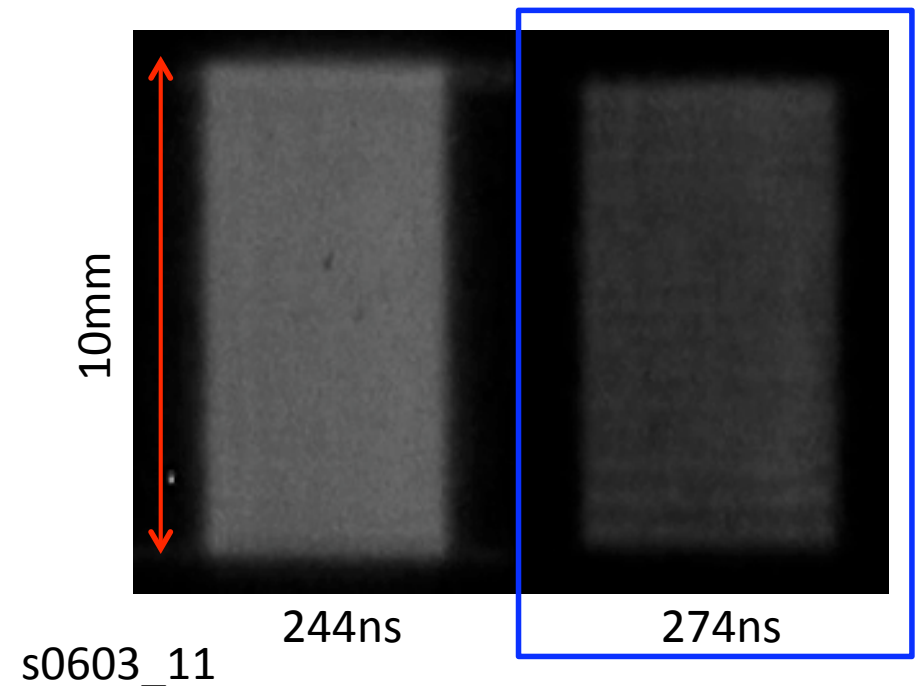


No anode-cathode asymmetry

Typically Ni liners light up 30ns earlier than Al liners

Correlated azimuthal striations seen on Ni liners at late times

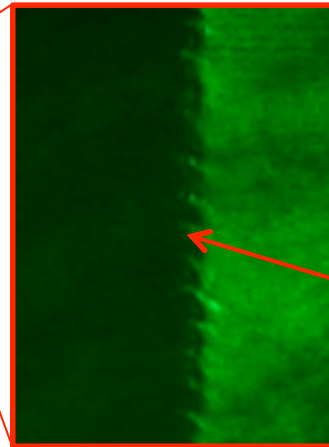
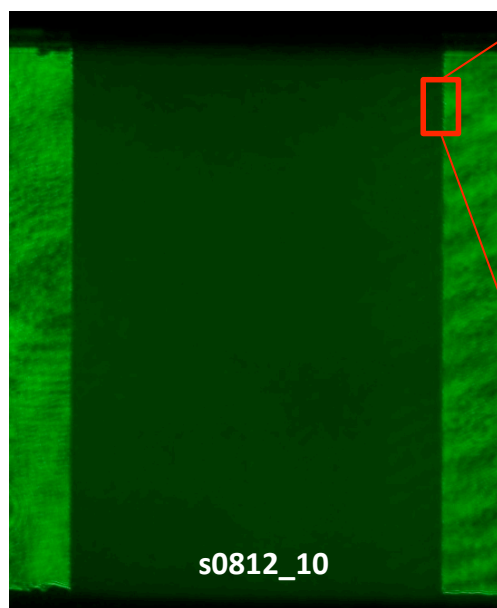
No XUV emission from 80um wall Al liners



Imaging the outside surface of liners

Laser probing of 20um wall aluminium liners

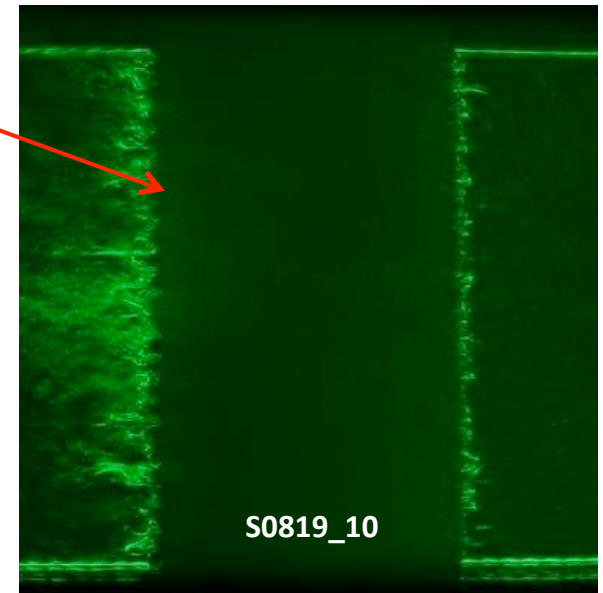
14mm diameter
Shadowgraphy 167ns



Seam position

$I \approx 170\mu\text{m}$
 $A \approx 110\mu\text{m}$

10mm diameter
Schlieren 298ns

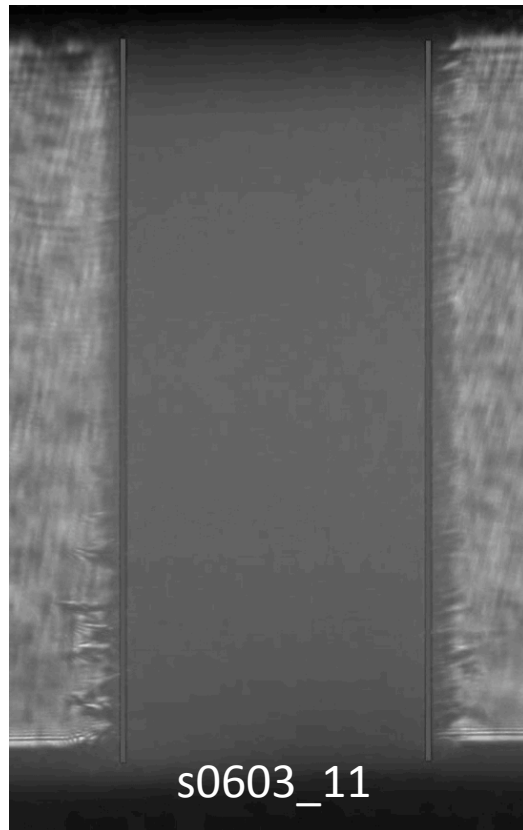


Small instabilities seen on surface of 20um aluminium liners

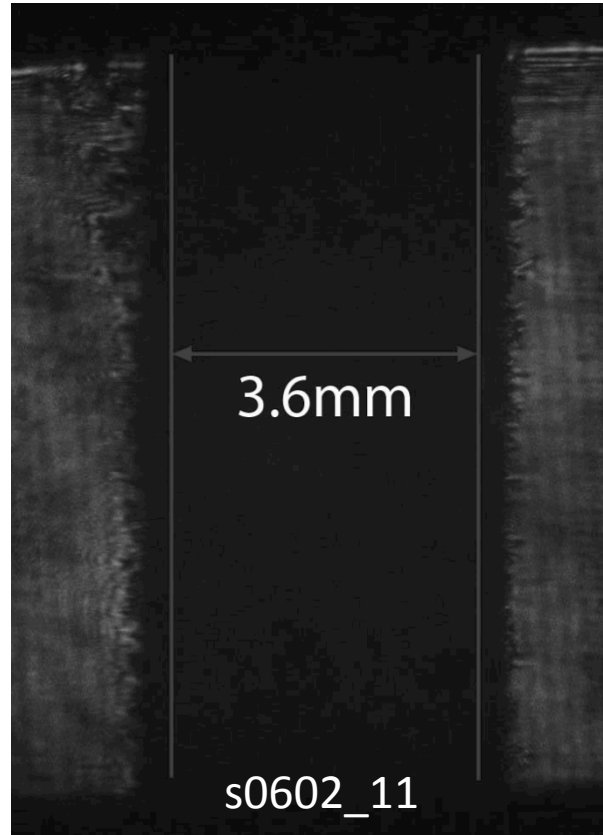
No plasma seen on outside of 80um aluminium liners

Imaging the outside surface of liners

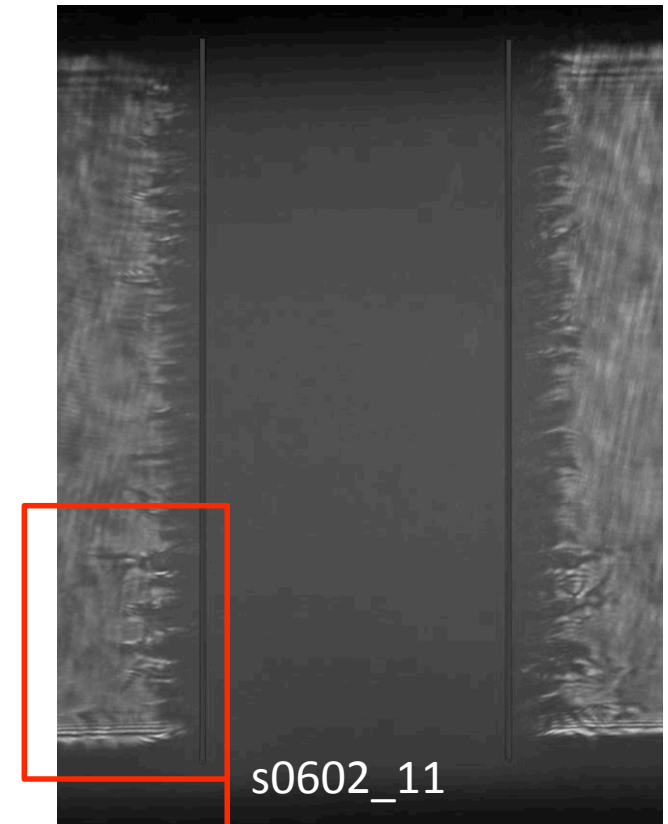
Shadowgraphy of 50 μ m wall nickel liners



169ns



227ns



247ns

$l = 300-400 \mu\text{m}$
Amplitude = 0.7-1.0 mm

Amplitude of instabilities grows at 10-15 km/s

Expansion velocity corresponds to $ZT_e = 2-4 \text{ eV}$

Liner parameters

	Ni 50um wall, 3.6mm OD	Al 20um wall, 14mm OD	Al 80um wall, 6mm OD
Resistivity (nΩm)	69.3	28.2	28.2
Skin depth (um)	90	60	60
Cross section (mm ²)	0.56	0.88	1.5
Mass per unit length (g m ⁻¹)	5	2.4	4
Melting point (K)	1728	933	933
Boiling point (K)	3186	2792	2792
Heat capacity (J mol ⁻¹ K ⁻¹)	26	24	24
Peak B field (T)	155	40	93